

14 HYDRODYNAMIC FORCES ON VERTICAL CYLINDERS  
15 AND THE LIGHTHILL CORRECTION

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18 Abstract—In the keynote address to the 1979 Behaviour of Offshore Structures (BOSS)  
19 Conference, Sir James Lighthill pointed out the absence of a second-order term of potential  
20 origin from the Morison description of the hydrodynamic force on a vertical cylinder. This  
21 term, referred to as the Lighthill correction, is due to the nonlinear interaction between the  
22 flow velocity and its horizontal gradient. As noted by Lighthill, if this term is omitted, the  
23 estimated drag force in the Morison equation is equal in effect to the actual drag force plus  
24 the Lighthill correction.

25 Thus, it would appear that in cases where hydrodynamic damping plays an important role  
26 and should therefore be estimated as accurately as possible, corrections of the Lighthill type  
27 might have to be added to the Morison expression for the hydrodynamic force. (One such case  
28 is the dynamic amplification of wind-induced fluctuating motions of tension leg platforms.) In  
29 particular, it might be expected that the estimation of the damping force would be more strongly  
30 affected in situations involving low Keulegan-Carpenter numbers, and therefore relatively low  
31 damping forces.

32 It is thus of interest to examine the effect of the Lighthill correction quantitatively. In this  
33 work, the expression for the Lighthill correction was derived for finite water depths.  
34 Measurements obtained in periodic wave flow at the Naval Civil Engineering Laboratory and  
35 in random wave flow at the Delft Hydraulics Laboratory were subjected to an extensive analysis.  
36 The results of the analysis showed that for both the periodic and random wave conditions and  
37 addition of the Lighthill correction (1) did not improve the Morison equation significantly, and  
38 (2) had no significant effect on the estimation of the drag force, including the drag force  
39 corresponding to very low Keulegan-Carpenter numbers.

40 INTRODUCTION

41 WAVE FORCES on cylindrical elements are of considerable interest in the design of  
42 offshore facilities. Morison *et al.* (1950) proposed a simple equation expressing the total  
43 wave force as the sum of two components: an inertia force, due to the effects of  
44 irrotational (potential) flow, and a drag force, due to viscosity (skin friction and flow  
45 separation) effects. The equation is calibrated with two empirical coefficients which are  
46 referred to as the inertia and drag coefficient and are functions of the flow conditions.

47 The Morison equation has been criticized as oversimplifying the fluid mechanics of  
48 the loading but an alternative rigorous approach has not been developed to date. There  
49 appears to be a consensus that, to represent the fluid mechanics more closely, it is  
50 better to add correction terms to the Morison equation rather than devise a completely  
51 new relationship (Keulegan and Carpenter, 1958; Lighthill, 1979; Sarpkaya, 1981; Cook,  
52 1987). The corrections of Keulegan, Carpenter and Sarpkaya are aimed essentially at  
53 accounting for vorticity effects. The topic of this paper, the Lighthill correction, is a  
54 correction associated with irrotational (potential) flow effects.

55 In his keynote address to the 1979 Conference on the Behaviour of Offshore  
56 Structures (BOSS) Sir James Lighthill showed that the force associated with the  
57 irrotational flow includes, in addition to the linear inertia term of the Morison equation,  
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